AD/A-001 720

THE DEGRADATION OF NYLON BY IRON RUST

Richard I. Tubis

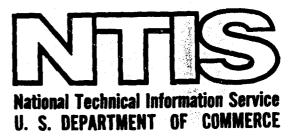
Naval Aerospace Recovery Facility

Prepared for:

Naval Air Systems Command

August 1974

DISTRIBUTED BY:



#### NOTICES

Qualified requestors may obtain copies of this report from the Defense Documentation Center, Cameron Station, Alexandria, Virginia 22314. Department of Defense contractors must be established for DDC services or have "need to know" certified by cognizant military agency of their project or contract.

DDC release to NTIS is authorized.

When U.S. Government drawings, specifications, or other data are used for any purpose other than a definitely related government procurement operation, the government thereby incurs no responsibility nor any obligation whatsoever: and the fact that the government may have formulated, furnished, or in any way supplied the said drawings, specifications, or any other data is not to be regarded by implication or otherwise, as in any manner licensing the holder or any other person or corporation or conveying any rights or permission to manufacture, use or sell any patented invention that may in any way be related thereto.

Do not return this copy; retain or destroy.

ACCESSION	for	
NTIS DDG UHAHHOUHG JUSTIFICAT	White Section Bull Section ED ION	0
BY	TICH/AVAILABILITY CO	DES
Dist.	AVAIL and or SPEC	IAL
A		

#### UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Date Entered)

REPORT DOCUMENTATION	PAGE	READ INSTRUCTIONS BEFORE COMPLETING FORM				
. REPORT NUMBER	2. GOVT ACCESSION NO.					
8-74		HD/HBO! 120				
4. TITLE (and Subtitle)		5. TYPE OF REPORT & PERIOD COVERED				
The Degradation of Nylon by Iron	Rust	Final				
		6 PERFORMING ORG. REPORT NUMBER				
7. AUTHOR(s)		NAVAERORECOVFAC 8-74  8. CONTRACT OR GRANT NUMBER(s)				
Richard I. Tubis						
9. PERFORMING ORGANIZATION NAME AND ADDRESS	· · · · · · · · · · · · · · · · · · ·	10. PROGRAM ELEMENT, PROJECT, TASK AREA & WURK UNIT NUMBERS				
Naval Aerospace Recovery Facilit	у	ALEX O WOLL SHIT MOMBERS				
El Centro, California 92243						
11. CONTROLLING OFFICE NAME AND ADDRESS		12. REPORT DATE				
Naval Air Systems Command		August 1974				
Washington, D. C. 20360		13. NIMPER OF PAGES				
washington, D. C. 2030		ર્સ એ				
14. MONITORING AGENCY NAME & ADDRESS(II dillere	nt from Controlling Office)	15. SECURITY CLASS. (of this report)				
·		UNCLASSIFIED				
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE				
16. DISTRIBUTION STATEMENT (of this Report)						
DDC Release to NTIS Authorized						
17. DISTRIBUTION STATEMENT (of the abstract entered	d in Block 20. if different fr	om Report)				
	,					
N/A						
NAT INFC	uced by IONAL TECHNICAL DRMATION SERVICE S Department of Commerce Springfield, VA. 22151					
19. KEY WORDS (Cantinue on reverse side if necessary	and identify by block number	r)				
Polyamide Rus	st	·				
Nylon						
Environmental Degradation						
Iron Oxide						
20. ABSTRACT (Continue on reverse side if necessary a Nylon (both fabric and cord) was						
environments of sea water (synth	netic), distilled	water, pH4 and pH10. The				
iron rust and Fe <sub>2</sub> O <sub>3</sub> were found t						
to the nylon. The FeCl <sub>3</sub> was deg	rading as expect	ted.				

# U.S. NAVAL AEROSPACE RECOVERY FACILITY El Centro, California

#### THE DEGRADATION OF NYLON BY IRON RUST

bу

Richard I. Tubis

This Technical Report has been reviewed and is approved:

D. DIRIAN

Head, Engineering Department

H.C. FISH

Technical Director

CAPT R.S. CKEW, JR. USN

Commanding Officer

#### ABBREVIATIONS AND SYMBOLS

cc Cubic Centimeter

FeCl<sub>3</sub> Ferric Chloride

Fe2O3 Ferric Oxide

HCl Hydrochloric Acid

KCl Potassium Chloride

NaBr Sodium Bromide

NaCl Sodium Chloride

NaOH Sodium Hydroxide

pH Logarithm of the Reciprocal of the Hydrogen Ion Concentration

σ Standard Deviation

 $\overline{X}_n$  Mean Value of Group n

 $\overline{\overline{X}}_n$  Mean of the Means of Group n

#### SUMMARY

This test program was conducted to resolve conflicting evidence as to whether or not iron rust is degrading to nylon. Two tests were conducted: the first used 1.1 oz. ripstop nylon and 50-lb. 6-cord; the second used 1.1 oz. ripstop nylon only. The test samples were divided into four groups: control, iron rust, Fe<sub>2</sub>O<sub>3</sub> and FeCl<sub>3</sub>. Each group was divided into five environments: dry, distilled water, salt water, pH4 and pH10. The samples were left in their specific environments for 30 days before being washed, dryed, and tested. It was determined that iron rust does not chemically degrade nylon to any significant degree.

## TABLE OF CONTENTS

Pag	gе
List of Tables	. <b>v</b>
Introduction	l
Test-Material-Equipment-Chemicals	1
Method of Tests	l
Discussion	2
Conclusion	3
Recommendation	4
APPENDIX A	
Individual Breaking Strengths 1.1 Ounce Ripstop Nylon-Test No. 1 !	5
APPENDIX B	
Individual Breaking Strengths of 50-Pound, 6-Cord Nylon Thread- Test No. 1	7
APPENDIX C	
Individual Breaking Strengths of 1.1 Ounce, Ripstop Nylon- Test No. 2	9

## LIST OF TABLES

Tab	<u>ole</u>		Pa	ige
I	Tabulated Results of Test I for 1.1 Ounce Ripstop Nylon			11
II	Tabulated Results of Test I for 50-Pound, 6-Cord Nylon Thread.	•		12
Ш	Tabulated Results of Test II-1.1 Ounce Ripstop Nylon			13

#### INTRODUCTION

Many users of aliphatic polyamide nylon cord, webbing, rope, and fabric have formed the opinion that iron rust degrades these articles in service.

An informal test program conducted at the NAVAERORECOVFAC (Naval Aerospace Recovery Facility) appeared to confirm this belief. However, later tests at the NAVAERORECOVFAC and U. S. Army's Natick Laboratories failed to support either the earlier test results or the opinion that iron rust was degrading.

The program reported herein was established in an attempt to resolve these anomalous results.

#### TEST-MATERIAL-EQUIPMENT-CHEMICALS

The test materials utilized were 1.1 oz. ripstop nylon (type 330) canopy fabric and 6-cord nylon thread both being manufactured from nylon 66 (polyhex-amethylene adipamide).

The test equipment consisted of a Fisher Accumet 420 pH meter, twenty 150 cc beakers, 14 one-quart mason jars, an Instron Tensile Tester, plus general laboratory equipment.

The chemicals used included NaOH solution, HCl solution, NaCl, NaBr, KCl, Fe<sub>2</sub>O<sub>3</sub>, FeCl<sub>3</sub>, distilled water and iron rust.

# METHOD OF TEST

Samples were exposed to five general test environments: (1) dry, (2) wet-distilled water, (3) wet-salt water (similar to sea water), (4) pH4 (HCl solution), and (5) pH10 (NaOH solution).

The latter three environments were prepared as follows: (3) Twenty grams of NaCl, 10 grams of KCl and 2 grams of NaBr were placed in 1000 cc of distilled water and stirred until dissolved. (4) A  $1 \times 10^{-4}$  normal solution of HCl which corresponds to a pH4 solution was prepared. The pH of the solution was taken and it was either diluted or additional acid solution added as needed to obtain approximately a pH4 solution. (5) A  $1 \times 10^{-4}$  normal solution of NaOH which corresponds to a pH10 solution was prepared. The pH of the solution was taken and it was either diluted or additional base solution was added as needed to obtain approximately a pH10 solution. (Note: The acid and base solution must be well stirred otherwise an incorrect pH reading will be obtained).

Test No. 1 One-hundred 1½-inch-wide by 8-inch-long samples of 1.1 oz. ripstop nylon, type 330, and twenty 40-inch-long samples of 50-lb., 6-cord nylon thread were prepared. Five ripstop nylon samples and one thread sample were placed in each of the twenty 150 cc beakers. Five beakers were used as the control group, five as the iron rust group, five as the Fe<sub>2</sub>O<sub>3</sub> group, and five as the FeCl<sub>3</sub> group. The five test environments for each group included dry, distilled water, salt water, pH4, and pH10.

To place the three chemicals (Fe<sub>2</sub>O<sub>3</sub>, Iron Rust, and FeCl<sub>3</sub>) on the samples, each piece of nylon was first wetted with distilled water and then rolled in the powdered chemical. The nylon samples were folded and placed in the appropriate beaker. After the nylon had dried, 30 cc of the designated solution (as shown on the beakers) was added to each beaker and allowed to stand for 30 days. During that time, distilled water was added as required to compensate for evaporation.

After the 30-day period, the samples were washed in a mixture of cold water, Tide, and Avitex AD and then rinsed and dried at room temperature. Each beaker sample group was placed in an individually marked envelope. The samples were environmentally conditioned under standard ambient conditions and their breaking strength determined by means of the Instron Tensile Tester.

Test No. 2: One hundred-twenty 1½-inch-wide by 8-inch-long samples of 1.1 oz. ripstop nylon, type 330, were prepared. The ripstop samples were placed in each of 10 of the 14 mason jars and five samples were placed in each of the other four jars. Five mason jars contained Fe<sub>2</sub>O<sub>3</sub>, and the remaining four contained iron rust. (Due to the small amount of the original lot of iron rust remaining, only five samples per jar could be used and the pH10 environment was eliminated.)

The final procedure was identical to that for Test No. 1, except the mason jars were sealed; thus, no water had to be replaced due to loss by evaporation.

#### DISCUSSION

Tables I and II contain tabulated results of Test No. 1 on 1.1 oz. ripstop nylon and 50-lb., 6-cord nylon thread. Individual breaking strength values appear in Appendix A and Appendix B, respectively. The average breaking strength of the ripstop samples for each environment indicated a slight decrease in strength from the controls to the Fe<sub>2</sub>O<sub>3</sub> and showed a large decrease to the FeCl<sub>3</sub>. The iron rust, however, did not follow this pattern even though iron rust consists mostly of Fe<sub>2</sub>O<sub>3</sub>. Since no significant change was apparent from the control

to the rust or  $Fe_2O_3$  as there was to the  $FeCl_3$  (a known degrader of nylon), test results were inconclusive. The standard deviations also revealed no specific pattern but remained random.

The 50-lb., 6-cord nylon thread samples showed the same general pattern i.e., slight reduction in breaking strength from the control to the Fe<sub>2</sub>O<sub>3</sub>. This time, however, the iron rust samples also followed the same pattern. The FeCl<sub>3</sub> proved to be degrading as was expected.

Standard deviations of the average breaking strengths for the controls, the rust, and the Fe<sub>2</sub>O<sub>3</sub> samples (omitting the FeCl<sub>3</sub>) were calculated for both the 1.1 oz. ripstop and the 6-cord. All the average breaking strengths were within +2 standard deviations (calculated for the three groups as a unit) for the 6-cord, and within +2.1 standard deviations for 1.1 oz. fabric. The hypothesis being that they all belonged to the same population group.

To clarify the results obtained, a second test was conducted on 1.1 oz. nylon ripstop using sealable mason jars to completely isolate each sample group from external conditions. Results of this test as shown in Table III, showed no drop in average breaking strength as occurred during the previous test. When standard deviations of the average breaking strengths were compared, they were all well within two standard deviations of the average as would be expected in a normal fabric breaking strength distribution curve. (For individual breaking strengths, refer to Appendix C.)

The majority of average breaking strengths for each test set were found to be slightly lower than the dry control of that set, indicating a detrimental albeit minute effect on the nylon.

Note that the breaking strength of nylon fabric may decrease due to the abrasive properties of powdered iron rust if not removed by washing (references 1 and 2). This may explain the prevalence of the belief that iron rust is degrading to nylon.

#### CONCLUSION

Although a slight loss in strength may result from prolonged (30 days or more) contact, iron rust cannot be considered as being chemically degrading to nylon to any significant extent. Strength losses noted in service are probably due to physical abrasive action of rust and associated contamination.

# RECOMMENDATION

All items of equipment fabricated wholly or partially of nylon and which come in contact with iron rust, should be washed in accordance with reference 3 to remove rust before degradation occurs.

# APPENDIX A.

Individual Breaking Strengths
1.1 Ounce Ripstop NylonTest No. 1

# Individual Breaking Strengths 1.1 oz. Ripstop Nylon-Test No. 1, lbs.

SAMPLE GROUP	SAMPLE	SAMPLE	SAMPLE	SAMPLE	SAMPLE
	1	2	3	4	5
CONTROL-Dry CONTROL-H <sub>2</sub> O CONTROL-Salt H <sub>2</sub> O	52.7	51.5	52.0	51.2	51.0
	52.2	53.2	52.0	53.2	51.2
	55.2	56.2	45.0	47.0	51.2
CONTROL-pH=4 (HC1) CONTROL-pH=10 (NaOH)	51.5	52.5	51.2	52.5	51.5
	50.7	50.2	48.0	51.2	51.0
RUST-Dry RUST-H2O RUST-Salt H2O RUST-pH=4 (HC1) RUST-pH=10 (NaOH)	52.0	47.7	51.2	50.5	53.0
	46.0	50.2	48.2	46.7	51.5
	54.2	54.5	53.0	55.0	54.0
	52.7	53.0	53.2	53.2	51.2
	53.0	48.2	53.0	51.5	49.7
FERRIC OXIDE-Dry FERRIC OXIDE-H <sub>2</sub> O FERRIC OXIDE-Salt H <sub>2</sub> O FERRIC OXIDE-pH=4 (HC1) FERRIC OXIDE-pH=10 (NaOH)	51.2 47.0 51.5 48.5 51.0	51.2 49.7 54.5 49.7 46.7	52.0 50.0 41.5 50.5 51.2	38.7	51.0 51.0 53.2 52.5 50.0
FERRIC CHLORIDE-Dry FERRIC CHLORIDE-H <sub>2</sub> O FERRIC CHLORIDE-Salt H <sub>2</sub> O FERRIC CHLORIDE-pH=4 (HCl) FERRIC CHLORIDE-pH=10 (NaOH)	32.0	36.0	33.0	39.0	32.5
	41.5	31.0	31.5	33.0	26.0
	13.7	15.2	17.5	41.2	42.0
	34.2	17.5	18.0	40.7	24.5
	20.2	40.5	42.0	13.0	18.0

## APPENDIX B.

Individual Breaking Strengths of 50-Pound, 6-Cord Nylon Thread-Test No. 1

TECHNICAL REPORT NO. 8-74

# Individual Breaking Strengths of 50-lb, 6-Cord Nylon Thread-Test No. 1, lbs.

SAMPLE GROUP	SAMPLE	SAMPLE	SAMPLE	SAMPLE	SAMPLE
	1	2	3	4	5
CONT'ROL-Dry	50.2	50.5	50.0	50.0	50.5
CONTROL-H2O	50.7		49.7	48.0	50.2
CONTROL-Salt H2O	51.5		50.5	52.2	51.2
CONTROL-pH=4 (HCl)	50.2		50.2	49.2	50.2
CONTROL-pH=10 (NaOH)	50.0	50.0	50.0	50.2	50.5
RUST-Dry	49.2	49.7	49.0	49.0	49.7
RUST-H2O	48.2	49.0	50. <b>0</b>	50.0	50.5
RUST-Salt H <sub>2</sub> O	46.7	48.0	51.0	50.7	44.0
RUST-pH=4 (HCl)	48.7	49.2	49.0	49.7	49.0
RUST-pH=10 (NaOH)	50.0	49.0	49.5	46.7	49.5
FERRIC OXIDE-Dry	49.2	49.5	49.2	49.5	49.0
FERRIC OXIDE-H <sub>2</sub> O	48.5	49.0	48.0	49.0	46.0
FERRIC OXIDE-Salt H2O	50.7	51.0	50.5	49.2	49.2
FERRIC OXIDE-pH=4 (HCl)	48.5	46.2	49.0	49.0	48.5
FERRIC OXIDE-pH=10 (NaOH)	48.2	48.5	49.0	48.7	49.2
FERRIC CHLORIDE-Dry	43.0	45.0	44.2	44.0	45.2
FERRIC CHLORIDE-H <sub>2</sub> O	45.0	44.2	45.5	45.0	45.0
FERRIC CHLORIDE-Salt H2O	45.7	45.0	42.7	46.0	44.7
FERRIC CHLORIDE-pH=4 (HCi)	42.5	40.0	42.0	43.0	43.0
FERRIC CHLORIDE-pH=10 (NaOH)	42.7	43.2	39.0	43.2	41.5

# APPENDIX C.

Individual Breaking Strengths of 1.1-Ounce, Ripstop Nylon-Test No. 2

Individual Breaking Strengths of 1.1 Ounce Ripstop Nylon-Test No. 2, Ibs.

	GROUP SAMPLE	-	8	8	4	₹	9	7	œ	6	10	==
	CONTROL-Dry	51.5	52.0	52.2	53.0	51.0	50.5	52.0	51.7	50.7	50.0	1
	CONTROL-H2O	53.0	51.2	47.7	50.5	51.7	52.0	50.5	51.0	90.05	1 1	1 1 1 1
	CONTROL-Salt	51.7	48.5	90.0	51.2	48.2	48.7	6.0.0	50.0	49.7	49.0	1
	CONTROL-pH=4	51.0	51.0	51.5	51.0	51.7	51.5	49.5	52.0	50.0	50.0	1
	CONTROL-pH=10	51.2	48.5	51.7	51.7	51.7	50.0	50.0	90.09	90.09	48.0 .	1
١.	RUST-Dry	51.0	48.2	51.0	53.0	52.0	1	1	1	i 1 1	1 1 1	1 6
	RUST-H2O	51.5	50.5	52.2	51.0	1 1 1 1	i i i	1	;	1	1 1	1
	RUST-Salt	52.2	51.0	51.2	51.2	50.5	51.2	1	!	1 1 1	1 1	;
	RUST-pH=4	50.0	51.0	52.7	51.2	51.5	!	1 1 1	1 1	1 1	1 1	1 1 1
	RUST-pH=10	1 1	1 1	1 1	{	1 1	; ; ;	1	1 1 4 1	1 1	1 1	1
	FERRIC OXIDE-Dry	52.0	53.0	52.0	49.7	50.5	52.0	48.0	52.5	50.2	52.0	!
	FERRIC OKIDE-H20	51.2	49.0	51.7	52.2	51.0	52.5	52.0	49.7	50.7	49.0	51.7
	FERRIC OXIDE-Salt	51.7	53.7	55.7	52.0	50.0	53.2	52.5	52.7	53.2	51.0	1 1
	FERRIC OXIDE-pH=4	52.2	52.5	51.7	52.5	52.0	53.0	52.0	52.0	52.2	51.2	53.0
	FERRIC OXIDE-pH=10	52.5	52.2	50.7	49.7	52.7	51.0	53.0	53.5	51.7	1 1	!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!

TABLE I: Tabulated Results of Test I for 1.1 Ounce Ripstop Nylon

		BREA	K STRENGTH (	LBS.)
	SAMPLE GROUP	RANGE	$\bar{\chi}$	σ
(1)	CONTROL-Dry	51.0-52.7	51.7	.61
	CONTROL-Distilled Water	51.2-53.2	52.4	. 76
	CONTROL-Salt Water	45.0-56.2	50.9	4.40
	CONTROL-pH=4	51.2-52.5	51.8	. 55
	CONTROL-pH=10	48.0-51.2	50.2	1.16
			₹ = 51.4	σ =.77
(2)	IRON RUST-Dry	47.7-53.0	50.9	1.79
(2)	IRON RUST-Distilled Water	46.0-51.5	48.5	2.07
	IRON RUST-Salt Water	53.0-55.0	54.1	.66
	IRON RUST-pH=4	51.2-53.2	52.7	.75
	IRON RUST-pH=10	48.2-53.0	51.1	1.88
			$\frac{x_1}{x_2} = 51.5$	σ = 1.85
(3)	FERRIC OXIDE-Dry	49.0-52.0	50.9	1.00
	FERRIC OXIDE-Distilled Water	47.0-51.0	49.7	1.47
	FERRIC OXIDE-Salt Water	41.5-54.5	49.4	4.81
	FERRIC OXIDE-pH=4	38.7-52.5	48.0	4.82
	FERRIC OXIDE-pH=10	46.7-51.2	50.0	1.72
			$\frac{\pi}{x_3} = 49.6$	$\sigma = .95$
			$\frac{1}{2}$ = 50.8	σ =1.56
(4)	FERRIC CHLORIDE-Dry	32.0~39.0	34.5	2.65
(4)	FERRIC CHLORIDE-Dry FERRIC CHLORIDE-Distilled Water	26.0-41.5	32.6	5.03
	FERRIC CHLORIDE-Distilled Water	13.7-42.0	25.9	12.90
		17.5-40.7	27.0	9.13
	FERRIC CHLORIDE-pH=4 FERRIC CHLORIDE-pH=10	13.0-42.0	26.7	12.10
	PERMIC ONDONIDE-PRI-10	13.0-44.0	20.1	12.10
			$\bar{\bar{x}} = 29.34$	$\sigma = 3.51$
			$\Xi_{X=45.5}$	σ =9.56

TABLE II: Tabulated Results of Test I for 50-Pound, 6-Cord Nylon Thread

		BREA	AK STRENGTH	(LBS.)
	SAMPLE GROUP	RANGE	$\bar{x}$	σ
(1)	CONTROL-Dry	50.0-50.5	50.2	. 23
	CONTROL-Distilled Water	48.0-50.7	49.7	.92
	CONTROL-Salt Water	50.5-52.2	51.4	. 56
	CONTROL-pH=4	49.2-50.2	50.0	.40
	CONTROL-pH=10	50.0-50.5	50.1	. 20
			$\overline{\overline{x}}_i = 50.3$	σ :.58
(2)	IRON RUST-Dry	49.0-49.7	49.3	. 32
ν-,	IRON RUST-Distilled Water	48.2-50.5	49.5	. 83
	IRON RUST-Salt Water	44.0-51.0	48.1	2.61
	IRON RUST-pH=4	48.7-44.7	49.1	. 33
	IRON RUST-pH=10	46.7-50.0	48.9	1.17
			<del>¯</del> - 49.0	σ =.48
(3)	FERRIC OXIDE-Dry	49.0-49.5	49.3	. 20
	FERRIC OXIDE-Distilled Water	46.0-49.0	48.1	1.11
	FERRIC OXIDE-Salt Water	49.2-51.0	50.1	. 7
	FERRIC OXIDE-pH=4	46.2-49.0	48.2	1.04
	FERRIC OXIDE-pH=10	48.2-49.2	48.7	. 40
			$\frac{\pi}{x}_{3} = 48.9$	σ =.74
			\(\bar{x}\) <sub>1,2\bar{3}</sub> 49.4	σ =.88
(4)	FERRIC CHLORIDE-Dry	43.0-45.2	44.3	. 79
	FERRIC CHLORIDE-Distilled Water	44.2-45.5	44.9	.42
	FERRIC CHLORIDE-Salt Water	42.7-46.0	44.8	1.16
	FERRIC CHLORIDE-pH=4	40.0-43.0	42.1	1.11
	FERRIC CHLORIDE-pH=10	39.0-43.2	41.9	1.59
			$\frac{1}{x_4} = 43.6$	σ=1.32
			$\frac{12.3.4}{2}$ = 47.9	<b>σ=</b> 2.70

TABLE III: Tabulated Results of Test II-1.1 Ounce Ripstop Nylon

		BREAK	STRENGTH (	LBS.)
	SAMPLE GROUP	RANGE	$\bar{x}$	σ
(1)	CONTROL-Dry	50.0-53.0	51.5	. 86
	CONTROL-Distilled Water	47.7~53.0	50.8	1.41
	CONTROL-Salt Water	48.2-51.7	49.7	1.08
	CONTROL-pH=4	49.5-52.0	50.8	.72
	CONTROL-pH=10	48.0-51.7	50.3	1.25
			₹,= 50.6	σ = .60
(2)	IDAN BUCT-D	48.2-53.0	51.0	1.60
(2)	IRON RUST-Dry IRON RUST-Distilled Water	50.5-52.2	51.3	.63
	IRON RUST-Distilled Water IRON RUST-Salt Water	50.5-52.2	51.2	.50
	IRON RUS"=4	50.0-50.7	51.3	.87
	IRON RUS1~pH=10	50.0-50.7		
	·		$\bar{\bar{x}}_{2} = 51.2$	σ = .12
(3)	FERRIC OXIDE-Dry	48.0-53.0	51.2	1.47
	FERRIC OXIDE-Distilled Water	49.0-52.5	51.0	1.19
	FERRIC OXIDE-Salt Water	50.0-53.7	52.3	1.15
	FERRIC OXIDE-pH=4	51.7-53.0	52.3	.43
	FERRIC OXIDE-pH=10	49.7-53.5	51.9	1.15
			\$ = 51.7	$\sigma = .55$
			$\bar{\bar{x}} = 51.2$	σ=.68

#### REFERENCES

- 1. U.S. Army Natick Laboratories Clothing and Personal Life Support Equipment, Report No. 70, "Strength Characteristics of Parachute Fabric dusted with Mica Powder." V.K. Devarakonda and J. Thompson, August 1972.
- 2. Naval Aerospace Facility Technical Note No. 10001-73, "Effect of Various Powders on Canopy and Container Fabrics." Kinloch, J.C.
- 3. Naval Air System Command, NAVAIR 13-1-6.2, "Manual-Aviation-Systems, Parachutes." November 1973.